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MM74C908 Dual CMOS 30-Volt Relay Driver

General Description

FAIRCHILD **SEMICONDUCTOR TM**

The MM74C908 is a general purpose dual high voltage driver capable of sourcing a minimum of 250 mA at $V_{OUT} =$ V_{CC} – 3V, and T_J = 65°C.

The MM74C908 consists of two CMOS NAND gates driving an emitter follower Darlington output to achieve high current drive and high voltage capabilities. In the "OFF" state the outputs can withstand a maximum of −30V across the device. These CMOS drivers are useful in interfacing normal CMOS voltage levels to driving relays, regulators, lamps, etc.

Features

- Wide supply voltage range: 3V to 18V
- \blacksquare High noise immunity: 0.45 V_{CC} (typ.)
- Low output "ON" resistance: 8Ω (typ.)
- High voltage: -30V
- High current: 250 mA

Ordering Code:

Connection Diagram

Absolute Maximum Ratings(Note 1)

Lead Temperature (T_L) (Soldering, 10 seconds) 260°C Power Dissipation (P_D) Refer to Maximum Power

Dissipation vs Ambient Temperature Graph

Note 1: "Absolute Maximum Ratings" are those values beyond which the
safety of the device cannot be guaranteed. Except for "Operating Tempera-
ture Range" they are not meant to imply that the devices should be operated at these limits. The Electrical Characteristics table provides conditions for actual device operation.

DC Electrical Characteristics

Min/Max limits apply across temperature range, unless otherwise noted

AC Electrical Characteristics (Note 3)

Note 3: AC Parameters are guaranteed by DC correlated testing. **Note 4:** Capacitance is guaranteed by periodic testing.

Power Considerations

Calculating Output "ON" Resistance (R_L > 18Ω)

The output "ON" resistance, R_{ON} , is a function of the junction temperature, T_J , and is given by:

 $R_{ON} = 9 (T_J - 25) (0.008) + 9$: (1)

and T_1 is given by:

 $T_J = T_A + P_{DAV} \theta_{JA}$; (2)

where T_A = ambient temperature, θ_{JA} = thermal resistance, and P_{DAV} is the average power dissipated within the device. P_{DAV} consists of normal CMOS power terms (due to leakage currents, internal capacitance, switching, etc.) which are insignificant when compared to the power dissipated in the outputs. Thus, the output power term defines the allowable limits of operation and includes both outputs, A and B. P_D is given by:

$$
P_D = I_{OA}^2 R_{ON} + I_{OB}^2 R_{ON}
$$
, (3)

where I_O is the output current, given by:

$$
I_{O} = \frac{V_{CC} - V_{L}}{R_{ON} + R_{L}}
$$

 V_L is the load voltage.

The average power dissipation, P_{DAV} , is a function of the duty cycle:

 $P_{DAV} = I_{OA}^2 R_{ON}$ (Duty Cycle_A) + (5)

 I_{OB}^2 R_{ON}(Duty Cycle_B)

where the duty cycle is the % time in the current source state. Substituting equations (1) and (5) into (2) yields: $T_{\rm J} = T_{\rm A} + \theta_{\rm JA}$ [9 (T_J – 25) (0.008) + 9]: (6a)

 $[I_{OA}² (Duty Cycle_A) + I_{OB}² (Duty Cycle_B)]$

simplifying:

(4)

 $T_J = \frac{T_A + 7.2 \text{ }\theta_{JA}\text{ }[I_{OA}^2 \text{ (Duty Cycle}_A) + I_{OB}^2 \text{ (Duty Cycle}_B)]}{1 - 0.072 \text{ }\theta_{JA}\text{ }[I_{OA}^2 \text{ (Duty Cycle}_A) + I_{OB}^2 \text{ (Duty Cycle}_B)]}$

Applications

(See AN-177 for applications)

Equations (1), (4), and (6b) can be used in an iterative method to determine the output current, output resistance and junction temperature.

Assuming $R_{ON} = 11\Omega$, then:

$$
I_{OA} = \frac{V_{CC} - V_L}{R_{ON} + R_{LA}} = \frac{15}{11 + 100} = 135.1 \text{ mA},
$$

$$
I_{OB} = \frac{V_{CC} - V_L}{R_{ON} + R_{LB}} = 135.1 \text{ mA}
$$

and

$$
T_J = \frac{T_A + 7.2 \theta_{JA} [I_{OA}^2 \text{ (Duty Cycle}_A) + I_{OB}^2 \text{ (Duty Cycle}_B)]}{1 - 0.072 \theta_{JA} [I_{OA}^2 \text{ (Duty Cycle}_A) + I_{OB}^2 \text{ (Duty Cycle}_B)]}
$$

 $25 + (7.2) (110) [(0.1351)^{2} (0.5) + (0.1351)^{2} (0.75)]$ $T_{\rm J} =$ $\frac{1}{1-(0.072)(110)[(0.1351)^2(0.5)+(0.1351)^2(0.75)]}$ $T_J = 52.6$ °C and $R_{ON} = 9 (T_J - 25) (0.008) + 9$

$$
= 9(52.6 - 25) (0.008) + 9 = 110
$$

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